EE 3657 Final - Dec 8, 2008

1. A unity feedback system has a feedforward transfer function given by $G(s) = \frac{1}{s(s+1)}$. A series compensator of the form $\frac{s+3}{s+5}$ is designed. Calculate for both the uncompensated and compensated system the location of the dominant closed-loop poles and the

sated and compensated system the location of the dominant closed-loop poles and the static velocity error constant K_v . (Hint: Non-dominant root for compensated system is at s = -4.9006) (40)

Uncomp: $s^2 + s + l = 0 \implies s = (-1 \pm \sqrt{1-4})/2$, $k_V = \lim_{s \to 0} \frac{6}{5}$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: $s(s+1)/(s+5) + (s+3) = 0 \implies s^3 + 6s^2 + 6s + 3 = 0$ comp: s(s+1)/(s+5) + (s+3)/(s+5) + (s+3)/(s+5) + (s+3)/(s+5) comp: s(s+1)/(s+5) + (s+3)/(s+5) + (s+3)/(s+5)s(s+1)/(s+5)

2. In a sample question, we saw that the resonant frequency ω_r for an underdamped system $G(j\omega) = \frac{1}{1 + 2\zeta \left(j\frac{\omega}{\omega_n}\right) + \left(j\frac{\omega}{\omega_n}\right)^2}$ is given by $\omega_r = \omega_n \sqrt{1 - 2\zeta^2}$. Write a general expression for the phase angle of $G(i\omega)$ and then find its expression at the

general expression for the phase angle of $G(j\omega)$ and then find its expression at the resonant frequency. (20)

$$\underline{\left(4(j\omega)\right)} = -\tan^{-1}\left(\frac{23\omega/\omega_n}{1-\omega^2/\omega_n^2}\right)$$

$$\frac{\left(\Delta(1\omega)\right)_{\omega=\omega_{r}} = -\int_{an^{-1}} \left(\frac{23 \, w_{n} \sqrt{1-23^{2}/w_{n}}}{1-w_{n}^{2} \left(1-23^{2}\right)/w_{n}^{2}}\right) = -\int_{an^{-1}} \left(\frac{23 \, w_{n} \sqrt{1-23^{2}/w_{n}}}{23^{2}}\right) \\
= -\int_{an^{-1}} \left(\frac{1-33^{2}}{3}\right) dv_{n}^{2} dv$$

3. Two systems have transfer functions given by: (1) $G(s) = \frac{s+1}{(s^2+2s+2)(s+3)}$, and (2) $G(s) = \frac{s-1}{(s^2+2s+2)(s+3)}$. For both the cases, what is the slope (express in dB/decade) and the phase angle of the bode-plot as $\omega \to \infty$. (20)

(1) Slope =
$$n-m = (2)(20) = 40dB/deeade$$
.
Phax angle = $-180^{\circ} = -270^{\circ} + 90^{\circ}$

(2) Slope =
$$n-m = (3-1)(20) = 40dB/olucade$$

Phan angle = $-270^{\circ} - 90^{\circ} = -360^{\circ}$

4. Label gain and phase margin on an arbitrary (a) Bode and (b) Nyquist plot. (20)

